

Hydraulics

3rd Year civil

First Term (2009 - 2010)

Chapter ()

- - 12/480 fridae_ - - 12/480 fridae_

والمعق لنظرى المراجة المراجعة المراجعة

Compare Between Each Of:

- 1. Manning and Chezy Eqs.,
- 2. Effect of vegetation and roughness on Manning Coeff.,
- 3. Effect of curvature with large and small radius on Manning Coeff.,
- 4. Canal and flume,
- 5. Chute and drops,
- 6. Shallow wide sec. and narrow deep sec,
- 7. Efficient sec. and economic sec.
- 8. Laminar and turbulent flow.
- 9. Rapidly varied flow and gradually varied flow,
- 10. Average normal velocity and shear velocity,
- 11. IR. and IR,
- 12. Actual shear stress and critical shear stress,
- 13. A, R, Y, Y, and Z,
- 14. Specific energy and total energy,
- 15. Velocity correction factor and momentum correction factor,
- 16. Alternative depths and conjugate depths,
- 1.7. Specific energy, Specific discharge and Specific force diagrams,
- 18. Critical, sub-critical and super-critical flow,
- 19. Ideal and Elastic fluids,
- 20. Newtonian and Non-Newtonian fluids,
- 21. Stream line, Streak line, Path line and stream tube,
- 22. Open channel flow and Pipe flow,
- 23. Steady and Unsteady flow,
- 24. Uniform and Non-uniform,
- Effect of viscosity and effect of gravity,
- 26. Geometric, kinematics and dynamic similarity,
- 27. Permissible and critical tractive forces,
- 28. Dimensionally and non-dimensionally homogeneous,
- Hydraulically smooth and Hydraulically rough surface and
- the bed canal slopes.

Hanning egn. Q= 1. As/3 - 51/2 V = 1. R2/3. 51/2

chezy edn.

Q = C. A. VR-S cisEN

V = C. \R.5

Effect of Vegitation ENDUSTED 13 (N) delet Fire V-R = 1. R 3. 5/2 Effect of Roughness

in abole (n) post

Q= + AS/3 - 51/2

(n) جاده معامل کوی و به الحاده ترداد نامه (N) زیاده نظاء کی اس دا تمل لفناه مرداده و (N)

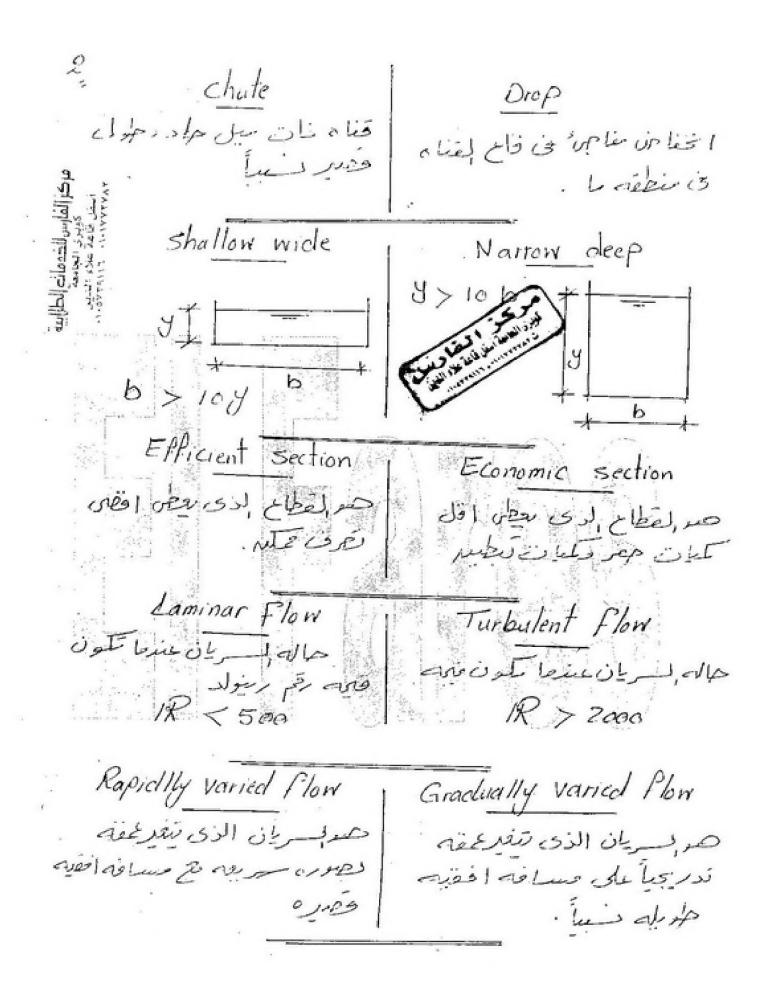
Curve with large radius - مزیاره نصف دعر دوران بایدی (n) हिंगी की कि

Curve with small rachius سعيان عيف قصر دران لادى

(ا مغدام معسان حاده) يزراد ا معامل طانتر

Canal

Flume قاء أحقن فالمعل



normal Velicity

Brish Less Leces

Alle Control

Brish Control

Brish Control

Brish Control

Brish Control

shear Velocity
هم فاءه السرعه داخل الفطاع ولاق المذبعة المربعة في المربعة في المربعة في المربعة في المربعة

المنز على المانز على

الدرى داخل المفطاع عن سرده (Shear Velocity)

R.

مدوره اجهار العقاد المحل المردى المحديث المردى المحديث المردى ال

Critical shear stress هم أ مقى الإلوقان تقلم لم مسان الدب دا المراب قطاع قبل أم تسا ق بحرك مع اتحاه لسريان

 $R = \frac{A}{P}$ A = (B + ZY)Y $\Gamma = B + ZY \sqrt{1+Z^2}$

z = A Vyh yh = 4 العَمَانِ المَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِ الْمَانِدِ الْمَانِي الْمَانِدِ الْمَانِدِ الْمَانِدِ الْمَانِي الْمِنْ الْمَانِي الْمِنْ الْمِنْ الْمَانِي الْمِنْ الْمَانِي الْمِنْ الْمَانِي الْمِنْ الْمَانِي الْمَانِي الْمَانِي الْمَانِي الْمَانِي الْمِنْ الْمِنْ الْمَانِي الْمِنْ الْمَانِي الْمِنْ الْمَانِي الْمِيْنِي الْمَانِي الْمِنْ الْمَانِي الْمِ

Total Energy

alia discourse Laboration

or significant consisted as a significant consisted and the significant consisted as a s

Energy Correction factor

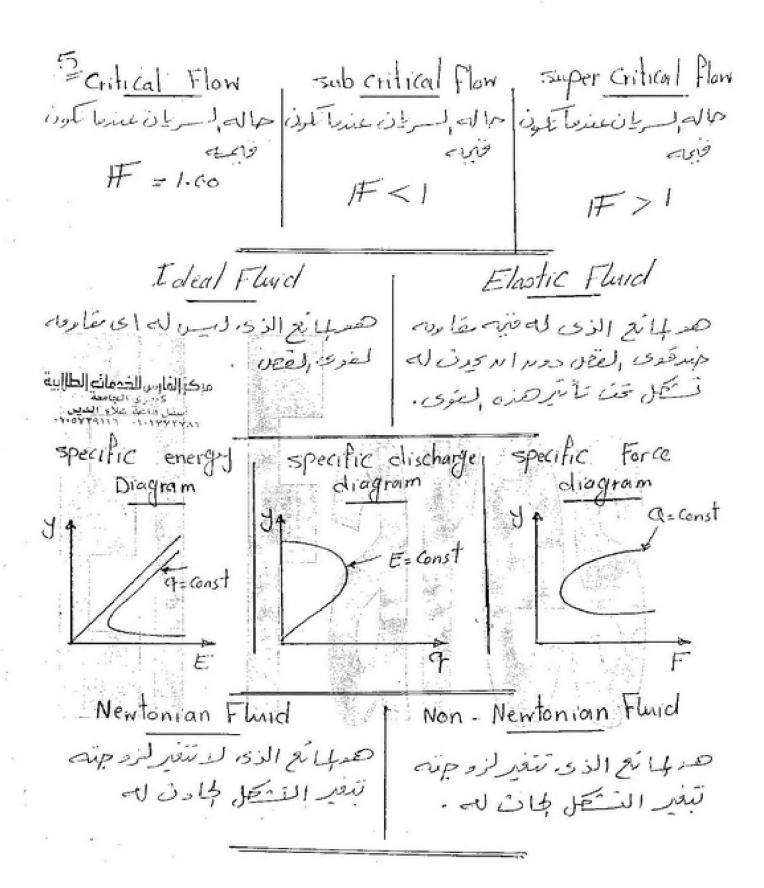
Momentum Correction factor عد عامل دَع و المحراث (B) معادله تلبط التحرك (B) المحرك عليه التحرك (B)

Alternative Depthes

Out per interior Legion Legion

Conjega te Depthes

Asign is which will so with the same of the sa



Stream Line streak line Path line stream tube صرافظ إذى ترسه صداخط لذي عل (300) 1000 Sec. 1000 No 03, 200 سرجمع لنفاط تحل إسران عراء عزى واعد وغوط السران النئ نمر ونقطه العلماس لله لعطى خلال فازه زمندے ورلى تعطى تقبل اتحاه السرده السنيه السراين open channel Flow Pipe Flow TEL T.E.L H.G.L H.G.L ١. ح يون العظاع معين ١- حيث نه العظاع يا بنه ، حجل موزیم لسرعات متصر. > - سيّحل توزيج لسرعات ثابت. ٣- العاد لقطاع متعره ---٣- العاد الفظاع ٢ ينه ع السريان تحت تأثر الحادسه ٤ ـ إسران تحت تأثر الفغط un steady Flow Steady Flow صد لريان لذى لاتتعر حصافهه صربران الذى تتعرجهانهم تتغر الوقت. Jes Leen 3y +0, 3y +0 3 =0 , St =0

non-Uniform Flow · Uniform Flow حدبسريان الذى لاتنفر مهارضه ع السامة. 3x =0, 3x =0 $\frac{\partial y}{\partial x} \neq 0$, $\frac{\partial y}{\partial x} \neq 0$ Effect of Gravity Effect of Viscocity ىرالجاذبىيى على IF = V Geometric Similarty Kinematic Similarty, Dynamic Similarty وتعقدصده لما تله على العقرصده لمعائله على تعقدصده لمحائله على نظل لعثوى نسب انظل للدبعاد يبسبه لعل لسرقه والعكوف 041 Fr= +m
FR 2r = 4m Permisible T.F | Critical T.F معاوفتى قومسى داخل ا حدقه قوه اسعب طعل لعظاع المجرى 4 اى قبل أم تبدأ بعصا مهاى لدى تدى معوا حركه لحبيبات حبيبات الترب في لحركه مع ا تجاه الكرب مع ا تجاه لسريان. السريان

Dimensionally
hemogenous

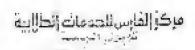
صابعادلة الذ تكون ضوالعاد
الطرفييرملساريه

non - Dimen sionally
hemogenous
عن المعادلة الذ تكون منها العاد ا

| Hydraulically Smooth | Hydraulically Rough |
|--|--|
| عنيعا تلون الحشونه بالمونه لفاع | عنيما تكون ارتفاع لجنثونه داخل |
| العناه ا فل عبر الحيثوره لمرجه | المجرى المائ آلبرصد لجنثونه |
| T T Ke | K>Kc dp , dl |
| | 100 Page 100 200 200 200 200 200 200 200 200 200 |
| | |
| Bed canal slopes: | |
| 10000000000000000000000000000000000000 | sc (Mild slope) |
| 50 5 | |
| 事 · So S | sc (steep slope) |
| So = 0 | (Horizontal) |
| 50 >0 | (Adverse slope) |
| | |

Define the Following Parameters :

- Discharge rating curve,
- 2. Ultra rapid flow,
- Types of open channels according to physical poundaries,
- Best hydraulic section.
- 5. Dimensions of Chezy coefficient
- 6. Isovels,
- 7. Factors affect Manning coefficient,
- 9. Drag coeff.
- 10. Potential head,
- 11. Critical depth line,
- 12. For critical flow y -- -- , IF-- -- , IF -- -- , q -- -- and F -- -- ,
- 13. For super-critical flow y()Ye, IF()1.0 and V is ---,
- 14. for rectangular sec. Ye=---, Ve=---- and Emin.=---,
- 15. Hydraulic jump,
- 16. Energy loss through jump,
- 17. efficiency of the jump,
- 18. Relative energy loss of the jump,
 - 19. Advantages and disadvantages of modeling,
- 20. Types of similarity,
- 21. control section,
- 22. brink depth, and Yb= ---- Yc
- 23. Bed canal slopes,
- 24. Regimes of flow,
- 25. Sub-critical-Laminar flow,
- Dimension analysis,
- 27. Roughness height,
- 28. Laminar sub-Layer,
- 29. Incipient motion,
- 30. Celerity,
- 31. Total energy line,
- 32. Dynamic equation of gradually varied flow and
- 33. Stagnation point.







Discharge rating curve هد محنی متم السّاده لهل Current meter 1 1 45 0 12 للعرف سرعه إسريان ععرفه عدلفات الحطرز ultra rapid Flow: (Super Critical flow) مرسران لذی تلون فنه فاته ما دی ا Types of Canals according to physical poundaries. 1 - natural Canals قان مسعم 2 - Artificial Canals قسوات حساعين Best Hydraulic section: معد لقطاع لذى معن ا دفي تعرف مع ا ولي عبل عند ap Lul is his Dimensions of chegy Geff. . · V=C. VR.5 : L.T-1 = C x V= x1 C=212+-1 L.T-1 = C. L'12

> scanner by : mahmoud ashraf titanic_ship1912@yahoo.com

Isovels: artimet pleis un bis de l'alle l'es à de ma l'éla فى بسرعه (داخل القطاع العرفتي للجرى بائ) · Factors affecting Manning Coeff. (n): 1 - Surface roughness. 2 - Vegetation. Eled Jels () in paper 3 - Canal irrigularties - ribel plevipus 4 - Canal alignment. olies, les 5 - Silting and slouring ist Jelscuring 6- obstruction is 45 Jels per Jels V* = 18.R.5 = 12/P Drag Coeff. : ص منهه قوى لفض المناقه صر السريان على بطدود

الصلب للقطاع بمائ وكو ترفي نضب اتجاه مجركه.

scanner by a mahmoud ashraf titanic_ship1912@yahoo.com

| Potential head: |
|--|
| ها ونه طامت العرفع السريان مقاسه صر مستوى |
| E=Z+y+ V2 (Z) on 10 |
| Critical depth line: |
| |
| صداحل لصندسه الذي تقع عليه كل النفط التي عسم |
| H= 1000 and 15 sol 15 - 100 and 15 - 1 |
| - J |
| مركز الفارس لاحتمان الطالبية |
| TOUT THE STATE STA |
| E |
| For Critical Flow. |
| - 8 = 8c , F = 1.0 , E = Emin = 1.5 yc |
| 9=9max , F= Fmin = 1542 |
| |
| For super Critical Flow: |
| y < Jc , F>1 , V is max. |
| For rectangular section: |
| 4- 3 92/a 2 Finin = 1.5 4c |

Hydraulic Jump:

جى ظاهره هسروليليه تحدث نتجه انتقال السريان مس sub critical alpol super critical alp

Energy loss through Jump. L-hL hL = E, -Ez Ei صى عدر لطاف الذي تم Ez osee Just Jessin

Effeciency of the Jump: حرقدره العفره التفسير للله على تشت الطاق طافل

2 = E2

Relative energy loss of Jump.

autinal osee, Jet au + abb pur mind, co والطافة الدستياسة للقفزه hL_

Advantages of modeling ١- التشاف سيرب لمنسأ. ى دورى تكاليف الدساء ٣- درا سيرحالات محال عفده

Disadvantage ١- عمل , لمعاذج مقلف >- بعد العوى ليعلم عسلوا معلماً میک (برجوبه - *بزلاز*ل - ...

| ~ | - |
|----|--------|
| ١ | 5 |
| 4 | |
| 94 | - part |

Types of similarity: 1- geometric similarity

2 - Kinematic similarity.

3 - Dynamic Similarity

Control section.

صر العظام الذي على تلوين العمر المحرج الحاد ما جله مستخدم في قبياسون البعرف

* Brick depth yb = 0.7 ye

Regimes of Flow.



صحریق تستیم لتصنیی انواع اسریان اعتماداً علی A> F فی بعس العقب

Sub Critical Laminar Flow:

حسو لسريان الذى تكون فنب

F<1

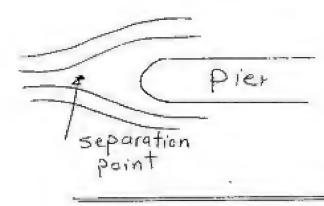
R < 500

Dimension analysis: 14 صرطريقة تستن لربط إعتدان إختلفه إوثره على ظامره ما واليجاد العلاقات بسيم حكنه لمتغيرات. Roughness height. تصومقار ارتفاع المنشونه بلونه كحوانث وقاع الحارى au (1) Laminar sub layer: ها ويته المريان بالقرب صر قاع لعناه ومنعل سلوم لسرطان سيرا في Incipient motion: هى بديه حركم حبيبات لكريه داخل الفناه وتتدأ عنوما رَعِلَ فَيْهِ فَقُوهِ, لَسُونَ وَاجْلَ لِجَرِي إِلَى إِلَى الْفَيْدَ كِمْرُ جِنْ Celerity: رعه انتقال إوجهي لمياه العادلة Total energy Line: صورخط سسم فيه الطاقه العليه راجل الحرى لماي

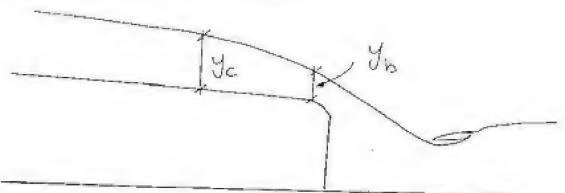
عنداى قطاع

Dynamic equation of G.V.F. ص العادلة التى تستم لايجاد العلاقة سيم عمراء رتغيره Jen 1940 or 3 levas outes aisest, as Lunt 20 50 - Se 1 + 29 dy Stagination Point: صى النقطم التي تقل سنهما سيرعه لسيريان إلى العفر وتحدث اجام البوابا ب Stagination Point Separation point:

عدد التي سا عنصا انعمال مطرط إلى المارى.



16 velocity Head: حمرجزء مسر لطاف ينهج مس انتقال إسريان سبريه (V2) casas (V) Los lies Relative initial depth: صربسبرسم الحمر لدسّائ للقفرة الصيروليكية م الطافات عند سانه القعزة (J:/E) Dimension of Manning Cotff.: .. V= + R2/3.15/12 $2.7 = \frac{1}{n} \cdot \left(\frac{2^2}{1}\right)^{2/3}$ L.T -1 = 1 2/3 n = 1-1/3.7 Current meter: صرعور ستخم لتحديد سيرعه باعداجل لقنوات



Jc = 07 Jb

Jc = 07 Jb

Jc = Jc = Jb = Jb = Jb = Jc

Jc = 4/g

Jc = 4 x B

Q = 4 x B

Defferent Models

Compare Between Each Of:

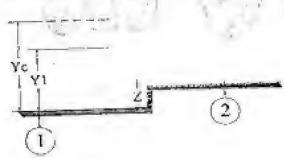
- Effect of vegetation and roughness on Manning Coeff.,
- Effect of curvature with large and small radius on Manning Coeff.,
- 3. Chute and drops,
- A. Shallow wide sec. and narrow deep sec,
- 5. Efficient sec. and economic sec,
- Rapidly varied flow and gradually varied flow,
- A. IR. and IR,
- 8. A, R, Y, Y, and Z,
- Specific energy and total energy,
- Alternative depths and conjugate depths,

Define the Following Parameters:

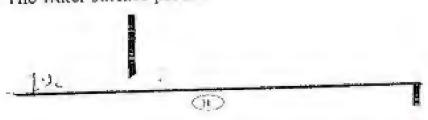
- Discharge rating curve, 1
- Ultra rapid flow, 2.
- Types of open channels according to physical boundaries, 13.
 - Best hydraulic section,
 - Dimensions of Manning coefficient, :5.
- Isovels, 6.
- Factors affect Manning coefficient,
- Drag coeff. 29.
- Potential head, _10.

Give Neat Sketch For Each Case:

1. The relationship between YI and Y2 and Z,



The water surface profile



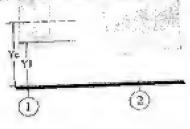
- Chute and drops,
- Shallow wide sec. and narrow deep sec,
- Efficient sec. and economic sec,
- IR, and IR.
- Actual shear stress and critical shear stress,
- Specific energy, discharge and force diagrams,
- Ideal and Elastic fluids,
- Open channel flow and Pipe flow,
- Effect of viscosity and effect of gravity on the flow,
- Geometric, kinematics and dynamic similarity,

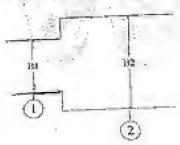
Define the Following Parameters:

- 11. Regimes of flow,
- 12. Sub-critical- Laminar flow
- 13. Dimension analysis,
- 14. Roughness height,
- 15. Laminar sub-Layer,
- 16. How a brink can be measure the discharge,
 - 17. Celerity
 - 18. Total energy line,
 - 19. Dynamic equation of gradually varied flow and
 - 20. Stagnation point.

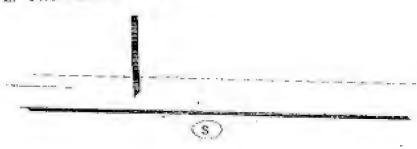
Give Neat Sketch For Each Case:

1. The relationship between Y1 and Y2 and B2,





The water surface profile



- 1. Normal velocity and shear velocity,
 - 2. IR. and IR.
 - 3. Actual shear stress and critical shear stress,
 - Specific energy and total energy,
 - Velocity correction factor and momentum correction factor,
 - Alternative depths and conjugate depths,
 - A. Critical, sub-critical and super-critical flow,
 - S. Ideal and Elastic fluids,
 - Newtonian and Non-Newtonian fluids,
 - 10. Open channel flow and Pipe flow,

Define the Following Parameters:

- 1. For critical flow y = -, IF = -, E = -, q = and F = -,
- 2. Energy loss through jump,
- Relative initial depth of the jump,
- 4. Types of similarity,
- _5. control section,
- _6. brink depth, and Yb-
- Bed canal slopes,
- = 8. Current meter,
- _9. Regimes of flow,
- _10: Sub-critical- Laminar flow,

Give Neat Sketch For Each Case:

The pressure inside the pizometer for each case,

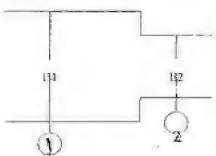


Convex

Concave

The relationship between Y1 and Y2 and B2, 3.





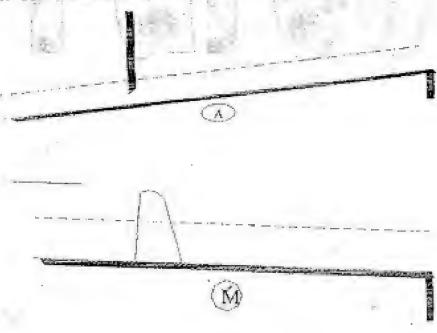
- A. Manning and Chezy Eqs.,
- 2. Canal and flume,
- 3. Efficient sec. and economic sec,
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- Newtonian and Non-Newtonian fluids,
- 8. Effect of viscosity and effect of gravity on the Flow,
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- 10. Hydraulically smooth and Hydraulically rough surface and

Define the Following Parameters:

- Discharge rating curve,
- 2. Best hydraulic section,
- 3. Dimensions of Manning coefficient,
- A. Drag coeff.
- 5. Potential head,
- 6. critical depth line,
- 7. For critical flow y = -, IF = -, E = -, q = and F = -,
- _8. for rectangular sec. Ye= ----, Ve= ---- and Emin.= ----,
- Relative energy loss of the jump,
- _10. Advantages and disadvantages of modeling, _.

Give Neat Sketch For Each Case:

The water surface profile



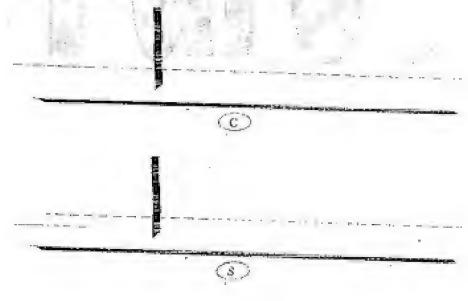
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- Alternative depths and conjugate depths,
- S. Specific energy, discharge and force diagrams,
- 9. Critical, sub-critical and super-critical flow,
- 10. Ideal and Elastic fluids,

Define the Following Parameters:

- 1. Ultra rapid flow,
- 2. Types of open channels according to physical poundaries,
- _3. Isovels,
 - 4. Factors affect Manning coefficient,
- 5. Velocity head,
- 6. For super-critical flow y()Yc, IF()1.0 and V is ---
- 7. Hydraulic jump,
- .8. Jump height,
- 9. efficiency of the jump,
 - 10. Relative initial depth of the jump,

Give Neat Sketch For Each Case:

1. The water surface profile



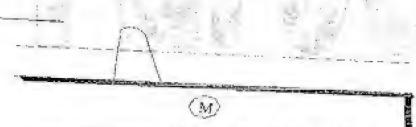
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 - 10. Stream line, Streak line, Path line and stream tube,

Define the Following Parameters:

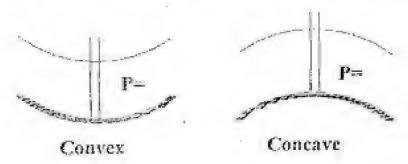
- 1. Types of open channels according to physical boundaries,
- 2. Dimensions of Chezy coefficient
 - 3. Isovels,
- .4. Critical depth line,
- 5. For critical flow y = -, F = -, q = and F = -,
- -6. For super-critical flow y()Yc, IF()1.0 and V is ----,
- _7. for rectangular sec. Ye= ----, Vc= ---- and Emin.= ----,
- _8. brink depth, and Yb= ---- Yc
- 9. Bed canal slopes,
- _10. Regimes of flow,

Give Neat Sketch For Each Case:

1. The water surface profile

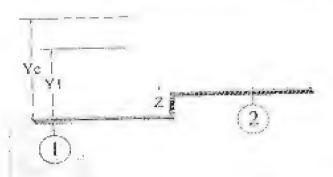


2- The pressure inside the pizometer for each case,

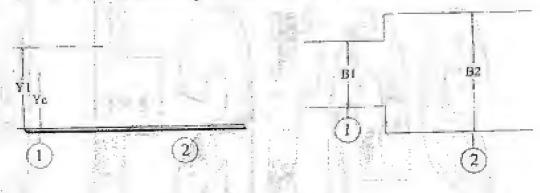


Give Neat Sketch For Each Case:

1. The relationship between Y1 and Y2 and Z,



2. The relationship between Y1 and Y2 and B2,



4. The water surface profile



- 1. Effect of curvature with large and small radius on Manning Coeff.,
- Canal and flume,
- 3. Chute and drops,
- Shallow wide sec, and narrow deep sec,
- 5. IR. and IR.
- A, R, Y, Y_h and Z,
- Stream line, Streak line, Path line and stream tube,
- 8. Open channel flow and Pipe flow,
- Geometric, kinematics and dynamic similarity,
- 10. Permissible and critical tractive forces,
- 11. Dimensionally and non-dimensionally homogeneous,
- Hydraulically smooth and Hydraulically rough surface and
- the bed canal slopes.

Define the Following Parameters:

- _12. For critical flow y = --, F = --, G = --, q = -- and F = --,
 - _13. For super-critical flow y()Ye, 1F()1.0 and V is ----,
 - _14. for rectangular sec. Ye=---, Ve=---- and Emin.=---,
 - -15. Hydraulic jump,
- 16. Energy loss through jump,
- _17. efficiency of the jump,
- 18. Relative energy loss of the jump,
- —19. Advantages and disadvantages of modeling,
- 20. Types of similarity,



MCQ on Open-Channel Flow

1. Open-channel flows have a pressure force driving the fluid similar to pipe flows. True or False

| | A. True |
|-----|--|
| L | S. False |
| | |
| | Where did the greatest difference between high and low tide occur? |
| سا | A. The Bay of Fundy, Canada |
| | B. Lundy's Lane, Canada |
| | C. The coast of Maine, U.S.A. |
| | Open channel flow can have more than one characteristic. True or False |
| ا | A. True |
| | B. False |
| 4, | The surface of a lake or ocean is often distorted into changing patterns associated with A. Evaporation |
| | B. Uniform flow |
| Ì | Surface waves |
| 5 n | nissing |
| 6. | The speed of a small amplitude, solitary wave is proportional to the of the fluid depth. |
| | Square root |
| 7. | The wave speed can be obtained from the continuity and energy equations. True or False c |
| | |

B. False

8. What does the term c represent in wave equations?

| ~ | A. Wave depth |
|-------------------|---|
| 5 | B. Wave speed |
| 2 | C. Amplitude |
| 9. How | is wave speed measured? |
| 5 | A. Relative to the flow |
| r | B. Relative to a fix position on the ground |
| £ | C. Relative to the acceleration of the wave |
| | at assumption is made about the slope of the channel bottom in most open channel flows? |
| E ₁₋₁₀ | A. The surface is rough. |
| L- | B. The slope is assumed to be constant. |
| 5 | C. The slope is assumed to be negative |
| | cording to the specific energy diagram, how many possible depths, with some physical meaning, there for given flow rate and specific energy, assuming $E > E_{min}$? |
| ~ | A. One |
| 15 | B. Two |
| £., | C. Three |
| | |
| | rate of change of the fluid depth depends on the local of the channel bottom, the of energy line, and the Froude number. |
| Ansv | |
| 1 | Slope Islope |

| 13. | How is uniform depth flow achieved? |
|-----|---|
| ١ | A. By adjusting the bottom slope to equal the slope of the energy line. |
| | B. By adjusting the flow speed so that it equals the energy line |
| | C. By ensuring uniform laminar flow |
| 14. | The wetted perimeter includes the free surface for open-channel flows. True or Fals |
| | A. True |
| | B. False |
| 15. | |
| | A. Along the entirety of the flow. |
| į | B. On the wetted perimeter. |
| | C. Only on the free surface |
| 16. | The velocity profile in an open channel is uniform. True or False |
| | A. True |
| | A. True |
| 17. | Are most open-channel flows laminar or turbulent? |
| | Turblent |
| 18. | The Manning equation is used to obtain the or flow rate in an open channel. A. Flow rate |
| | B. Density |
| | E C Velocity |
| 10 | The value of the Manning coefficient at depends on what? |

| | · |
|-------|--|
| - | A. The nature of the channel surface |
| < | B. The mass flow rate of the flow |
| . (| C. The type of fluid |
| | |
| 20. V | hat shape provides the best hydraulic cross section for open-channel flows? |
| 6 | A. A circular pipe |
| , • | B. A semicircular channel |
| - | G. A triangular channel |
| | |
| 21. V | What three classifications are open-channel flows divided into? |
| 1 | inswer: |
| 1 | wn, form depth, gradually Varying rapidly varying low many different surface shape designations are there for free surface calculations? |
| | rapidly varying |
| 22. 1 | low many different surface shape designations are there for free surface calculations? |
| | koswer: |
| | 12 |
| | 12 |
| ተነት ነ | On what two factors does the free surface shape depend on? |
| 23. | on what the meters does not |
| | The chainnel bottom slope and |
| , | The chainnel bottom slope and |
| | What is the technical term for a discontinuity in the free surface elevation of channel flow? |
| | A. A hydraulic jump |
| مسأ | |
| | B. A rectangular channel |
| | C. Rapidly varied flow |
| 25. | What is the primary cause of the head loss that occurs across a hydraulic jump? |
| | A. An increase in flow depth |
| | |

20.

Turbulent mixing C. A change in momentum

26. What function of the upstream flow dictates the depth ratio across a hydraulic jump?

A. The mass flow rate

B. The velocity of the flow

The Froude number

27. The length of a hydraulic jump can be determined analytically. True or False

B. False

28. What are the two main mechanisms governing the flow over a weir?

Inartia and growity

29. What happens to the velocity of the flow as it passes over a broad-crested weir?

A. It decelerates

Nothing

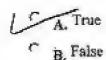
C. The flow accelerates and reaches critical condition.

MCQ on Dimensional Analysis, Similitude, and Modeling

| | to friction cannot generally be solved |
|------|---|
| 1. T | he pressure drop per unit length that develops due to friction cannot generally be solved nalytically. |
| ř | True |
| E | B. False |
| | |
| 2. | 4 qualitative description of physical quantities can be given in terms of |
| | A monitory |
| | Basic Dimension |
| | Dimensional analysis is the when the results of an equation will be what in relation to the system of |
| 3. | units chosen. |
| | S Dependent |
| , l | C B Independent |
| | |
| | C. Constant |
| | |
| 4. | Dimensional analysis is based on the |
| 7+ | |
| | Answer. |
| | Buckingham Pitheorem |
| | the dimensions of any |
| 5 | The dimensions of the variable on the left side of the equation must be the dimensions of any term that stands by itself on the right side of the equal sign. |
| | Eth Greater than |
| | B. Equal to |
| | C Fewer than |
| | C. |
| | |
| | 6. The required number of pi terms is what compared to the number of original variables? |
| | Greater than |

| | B. Equal to |
|---|--|
| | Se Eewer than |
| | 7. The most difficult step in the method of repeating variables is |
| | A. Listing all of the variables that are involved in the problem |
| • | B. Express each of the variables in terms of basic dimensions |
| | C. Determine the required number of pi terms |
| | The number of variables is desired to be kept to a minimum so that the amount of can be kept to a minimum. |
| | Laboratory work |
| | 9. When using the repeating variables method, the number of repeating variables that are selected should be what compared to the number of reference dimensions? |
| | C A. Greater than |
| | LC B. Equal to |
| | C. Less than |
| | 10. The pi terms must always be what? |
| | C A Negative |
| | B. Equal in dimensions |
| | C. Dimensionless |
| | |
| | 11. How many steps are there in the method of repeating variables? |

| 12. | If too many pi terms appear in the final solution then the problem may be difficult, time consuming, and to eliminate these experimentally. |
|-----|--|
| | Answer |
| | Expansive |
| 13. | Variables can be classified into three general groups: geometry, material properties, and external effects. |
| | CA. True |
| | B. False |
| 14. | An external effect is used to denote any variable that produces or tends to produce what? |
| | A. Inaccurate results |
| | B, Constant results |
| | Change in the system |
| | |
| | |
| 15. | How many different points are there to consider in the selection of variables? |
| | C A. 3 |
| ć | B. 6 |
| | C.8 |
| | C. C. |
| | |
| 16. | Typically, in fluid mechanics the required number of reference dimensions is |
| | Answer: |
| | The state of the s |
| | Three |
| | |
| 17. | Where does any other set of pi terms besides the original set come from? |
| | Answert |
| | Mam pulation of acorrected set of termi |
| | The number of required pi terms is fixed in accordance with the pi theorem. |



19. How many restrictions are there for pi terms?

A. None

Chree

20. Pi terms can be formed by inspection by simply making use of the fact that each pi term must be dimensionless.

A True B. False

21. Which of the following is equivalent to the repeating variable method?

Forming pi terms by inspection

B. Forming pi terms by dimensional analysis

C. Determination of reference dimensions

22. A useful physical interpretation can often be given to dimensionless groups.

A. True

B. False

23. Write the Reynolds number equation.

Rez PUL

24. What is the symbol for the Cauchy number?

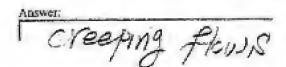
Cn A. Cn

| ستسا | B. | Ca | |
|------|----|----|---|
| C | C. | Cu | 1 |

25. The Weber number is a relationship between the inertial force and what other force?

Surface tension

- B. Kinetic
- C. Frictional
- 26. Flows with very small Reynolds numbers are commonly referred to as "_____".



- 27. The Euler number is undoubtedly the most famous dimensionless parameter in fluid mechanics.
 - C A. True

B. False

- 28. The Mach number and what other number cannot be used in the same problem?
 - A Euler number
 - B. Reynolds number
 - Cauchy number
- 29. The flow of river water is significantly affected by surface tension.
 - C A. True

B. False

30. The fewer the number of pi terms the more simple the problem.

A, True

| - | | |
|---|------|------------|
| 4 | 1875 | False |
| | W 6. | W. AND DAY |

31. For problems involving only two pi terms, results of an experiment can be conveniently presented in

· Asimple graph

32. For complicated problems it is often less feasible to use models to predict specific characteristics of the system than to develop general correlations.

A. True

33. A representation of a physical system that may be used to predict the behavior of the system in some desired respect is what?

A. Prototype

B. Model

C. Facsimile

34. Model design conditions are also called similarity requirements or modeling laws.

A. True

B. False

35. The second similarity requirement indicates that the model and the prototype must be operated at

The same Reynolds number

36. When velocity ratios and acceleration ratios are constant throughout the flow field, kinematic similarity exists between the model and the prototype.

A. True

G B. False 37. For true models, how many scales will there be? C A None B. One C. As many as needed 38. Models for which one or more of the similarity requirements are not satisfied are called _____ models. Auswer. Distorted 39. Distorted models cannot be successfully used, only true models can be accurately used. A. True R False 40. Geometric and Reynolds number similarity is usually not required for models involving flow through closed conduits. C A. True B. False 41. For large Reynolds numbers, the inertial forces are _____ the viscous forces? A. Less than B. Approximately the same as C. Larger than 42. For a Length Scale of 1/10 and a prototype velocity of 30 mph, what is the required model velocity?

ARSWOR

Boomp H

| 43. | How do the dimples on a golf ball effect drag? | |
|-----|---|------------------------------------|
| | They reduce drag | |
| | R, they increase drag | |
| | C. they do not effect drag | |
| | • | |
| 44. | When the Mach number becomes greater than approximatelybecomes significant. | , the influence of compressibility |
| | Аламег: | |
| | 0-3 | |

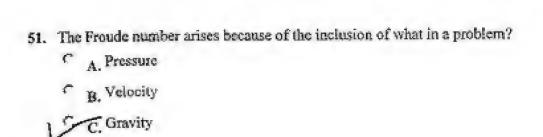


- 46. At temperatures of -20 °F, what is the ice growth rate that can be achieved.
 A. 1-mm per hour
 B. 2-mm per hour
 C. 3-mm per hour
- 47. The drag on a ship depends on both the Reynolds number and the Froutie number.

 A. True

 B. False

| 49. | or time-dependant problems, which of the following is crucial for successfully finding a solution |)DY |
|-----|---|-----|
| | A. The derivative of the equation | |
| t | B. Initial conditions | |
| | C. The velocities at all points | |
| 50. | Poverning equations expressed in terms of dimensionless variables lead to the appropriate limensionless groups. | |



B. False

52. From this section it can be concluded that for the steady flow of a compressible fluid without free surfaces, dynamic and kinematic similarity will be achieved.
A. True
False



Final Exam of Hydraulics 2009

Question (1)

| A) Hydraulically smooth | Hydraulically roughness |
|--|---|
| 1- Roughness don't effecting on velocity distribution 2-K<§o $\frac{u_* * k}{v} \prec 5$ $U = 2.5U_* \ln \frac{9yU_*}{v}$ | 1- Roughness effecting on velocity distribution 2-K>§o $\frac{\mu \cdot *k}{v} > 5$ $U \stackrel{?}{=} 2.5U. \ln \frac{30y}{k}$ |
| Best hydraulic section | Stable section |
| Its section is passing maximum discharge for minimum wetted perimeter at constant manning coefficient, water area and longitudinal slope. | -Its section not permissible to scouring or silling. |
| Friction velocity(shear velocity) | Mean flow velocity |
| its maximum velocity in channel before the particle of side and bed to move. $U_* = \sqrt{gRS}$ | Q=A*V Q=discharge m3/s A water area V Mean flow velocity m/s |
| State of flow | Regime of flow |
| When we study behavior of flow according to 1-effect of viscosity $IR = \frac{V * R}{v}$ $IR \le 500 \text{flow is laminar}$ $500 < IR \le 2000 \text{flow is transitional}$ $IR > 500 \text{flow is turbulent}$ $1-\text{effect of gravity}$ $FI = \frac{V}{\sqrt{g * y_k}}$ $F < 1 \text{flow is sub critical}$ $F = 1 \text{flow is critical}$ | When we take effect of gravity and viscosity the flow classified in the following cases 1-IR<500 & FI<1 flow is laminar-sub critical 2- IR<500 & FI >1 flow is laminar-superb critical 3- IR>2000 & FI <1 flow is turbulent-sub critical 4- IR>2000 & FI >1 flow is turbulent –super critical |

Given

A.S =65,000 fed

W.D=56 m³/fed/day

S=10cm/km

Z=1.00

n=0.025

Trapezoidal section

Rea

Design of sec for the following cases

1- V_{max}=0.58 m/s

2- ζ (max shear stress)=0.22kg/m²

Solutions

a) For maximum velocity
$$Q = \frac{A.S * W.D}{24 * 60 * 60} = \frac{65,000 * 56}{24 * 60 * 60} = 42.13....m^{3} / \text{sec}$$

$$A = y(b+zy) = 72.64....y(b+1*y) = 72.64....1$$

----By using manning equation

Get y=1.906 m & b=36.21m

b) For maximum shear stresses

ζ (max shear stress)=0.22kg/m²
ζ =γ*R*S
0.22 =1000*R*10*10*5R =2.2m

$$V = \frac{1}{2} * R^{\frac{2}{3}} * S^{\frac{1}{2}} ... m^{2} / sec V = \frac{1}{0.025} * (2.2)^{\frac{2}{3}} * (10*10^{-5})^{\frac{1}{2}}$$

V=0.667 m/s

$$Q = A * V \dots A = \frac{Q}{V} = \frac{42.13}{0.667} = 62.23 \dots m^2$$

----By using manning equation

$$Q = \frac{1}{n} * \frac{A^{\frac{5}{2}}}{p^{\frac{5}{2}}} * S^{\frac{1}{2}} ... m^{3} / \sec ... 42.13 = \frac{1}{0.025} * \frac{(62.23)^{\frac{5}{2}}}{(b + 2y\sqrt{1 + z^{2}})^{\frac{5}{2}}} * (10 * 10^{-5})^{\frac{1}{2}}$$

$$b + 2y\sqrt{1 + (1)^{2}} = 28.38... b = 28.38 - 2.83y... 2 \underline{Sub In 4}$$

$$62.27 = y(28.38 - 2.83y + y)... 62.274 = 28.385y - 1.83y^{2}$$

$$y^{2} - 15.44y + 34.03 = 0.00$$

Get v=2.663 m & b=20.84m

To compare excavation cost

1-By using max velocity

$$A = 72.64....m$$

2-By using max shear stress

$$A = 62.23...m^2$$

The cost of excavation in design by max excavation more than design by max shear stress

To show regime of flow

$$\frac{1-By \ using \ max \ velocity}{y_{h} = \frac{A}{T} = \frac{72.64}{(36.21 + 2*1.000*1.9063)} = \frac{42.64}{40.0226} = 1.0654m - FI = \frac{V}{\sqrt{g*y_{h}}} = \frac{[0.58]}{\sqrt{9.81*1.0654}} = 0.179 < 1.00$$
 sub...critical...flow

$$R = \frac{A}{P} = \frac{72.64}{\left[36.21 + 2*1.906\sqrt{1 + (1.00)^2}\right]} = \frac{68.6133}{41.6018} = 1.649$$

$$IR = \frac{V*R}{D} = \frac{(0.58)*(1.649)}{1*10^{-6}} = 956,586.35 \times 2000 \dots turbulent...flow$$

Flow is sub critical turbulent

1-By using max shear stress

$$y_{k} = \frac{A}{T} = \frac{62.23}{(20.84 + 2*1.000*2.663)} = \frac{42.64}{26.166} = 1.63m*$$

$$FI = \frac{V}{\sqrt{g*y_{k}}} = \frac{[0.667]}{\sqrt{9.81*1.63}} = 0.167 < 1.00....sub...critical...flow$$

$$R = \frac{A}{P} = \frac{72.64}{[20.84 + 2*2.663\sqrt{1 + (f.00)^{2}}]} = \frac{68.6133}{28.372} = 2.418$$

$$IR = \frac{V*R}{D} = \frac{(0.667)*(2.418)}{1*10^{-6}} = 1,612,806 > 2060....turbulent...flow$$

Flow is sub critical turbulent

Question (2)

A)

-specific energy

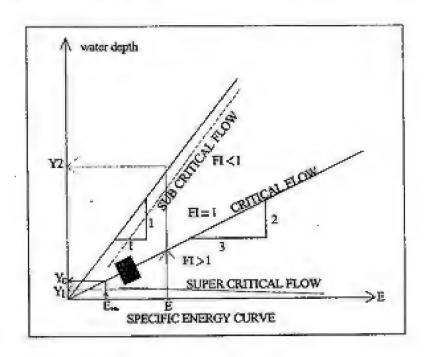
$$E = y + \frac{V^2}{2g} = y_2 + \frac{Q^2}{2 * g * A2^2}$$

-total specific energy

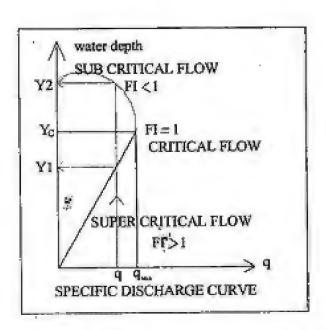
$$E = Z + y + \frac{y^2}{2g} = Z + y_2 + \frac{Q^2}{2 * g * A2^2}$$

-tow alternative depth

Its tow depths have the same specific energy and discharge one of them more than critical depth and occur in sub critical flow and other less than critical depth and occur in super critical flow



Specific energy diagram show relation between (E - Y) this curve draw under line slope 1: 1 (angle of 45°) there are anther line draw by slope 3: 2 (critical depth line) at y_c occurs minimum specific energy (yc =1.50 E_{min}). If y less than y_c flow is super critical and If y more than yc flow is sub critical.



Specific discharge diagram show relation between (q - Y) and at y_c occurs maximum specific discharge, if y less than y_c flow is super critical and if y more than yc flows is sub critical.

÷

<u>B)</u>

Given

Q=23m/s b =8.00m

&

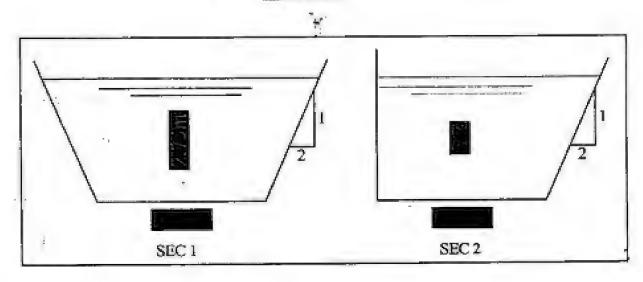
z =2 y=2.75m

Trapezoidal section

Required

1-water depth at contraction 2-max height of hump

Solution



1) To get water depth

Applying energy equation between section 1 and section 2 E1=E2+h_L

By neglecting head lose

$$A = y(b + zy) = 2.75(8 + 2 * 2.75) = 37.125....m$$

$$y1 + \frac{Q^2}{2g * A1^2} = y_2 + \frac{Q^2}{2 * g * A2^2}$$

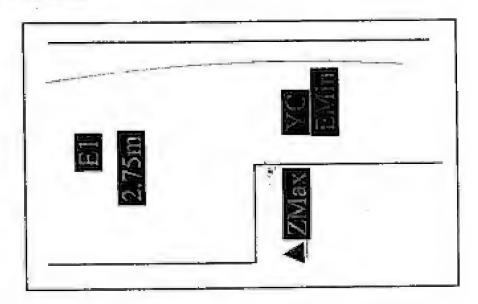
$$2.75 + \frac{(23)^2}{2 * 9.81 * 37.125^2} = y_2 + \frac{23.00^2}{2 * 9.81 * (6y_2 + y_2)^2}$$

$$2.7696 = y_2 + \frac{26.962}{(6y_2 + y_2)^2}$$

By trial and error

$Y_2 = 2.72m$

2- To get AZmex



E1=Emin+ AZmax

$$yl + \frac{Q^2}{2g + Al^2} = E_{min} + \Delta Z_{MAX}$$

$$E_{\min} = y_{\varepsilon} + \frac{y_{k}}{2}$$

$$\frac{Q^2}{Q} = \frac{A^3}{T}$$

$$\frac{Q^2}{g} = \frac{A^3}{T} \qquad \frac{(23.00)^2}{9.81} = \frac{(6y_e + y_e^2)^3}{(6+2y_e)}$$

$$53.925 = \frac{\left(6y_e + y_e^2\right)^3}{\left(6 + 2y_e\right)}$$

By trial and error

Yc=1.075m

$$y_k = \frac{n}{T} = \frac{(b + 2 * y_c)}{(b + 2 * y_c)}$$

$$y_h = \frac{A}{T} = \frac{\left(b * y_c * y_c^2\right)}{\left(b * 2 * y_c\right)} \qquad y_h = \frac{\left(6 * 1.075 + (1.075)^2\right)}{\left(6 * 2 * 1.075\right)} = 0.9332$$

$$E_{min} = y_e + \frac{y_h}{2} = 1.075 + \frac{0.9332}{2} = 1.5416m$$

$$E_{\text{edis}} = y_c + \frac{y_c(2.50 + 1.50y_c)}{2(2.50 + 2*1.50*y_c)} = 2.00$$

$$yl + \frac{Q^2}{2g * Al^2} = E_{min} + \Delta Z_{mix}$$

$$2.75 + \frac{(23)^2}{2*9.81*37.125^2} = 1.5416 + \Delta Z_{\text{max}}$$

$\Delta Z max = 1.2 m$

QESTION (3)

Open channel pipe 1-main force affecting on flow is inertia 1-main force affecting on flow is inertia force and viscosity force. force and gravity force. 2-main dimensionless number described 2-main dimensionless number described flow is Renold number low is Froude number 3- artificial 3-natural or artificial 4-for IR≤500 flow is laminar 4-for IR≤200 flow is laminar 2000<IRs4000 flow is transitional 500<IRs2000 flow is transitional IR>2000 flow is turbulent IR>4000 flow is turbulent 5shear distribution Velocity distribution shear distribution Velocity distribution VELOCITY DISTRESUITION NAME SPEAK DISTRESUITON NAME

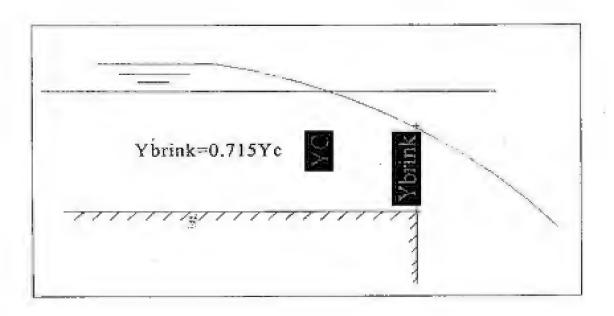
B)

-Tow conjugate depth

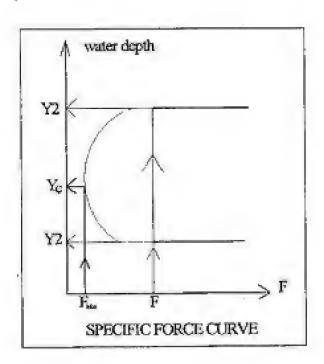
Its tow depts. h have the same specific force one of them more than critical depth and occur in sub critical flow and other less than critical depth and occur in super critical flow. And occur together.

-Control section

Its section at which water depth equal critical depth



-Specific force



Specific force diagram show relation between (F - y), y_c occurs at minimum specific force. If y less than yc flow is super critical and If y more than yc flow is sub critical. These tow depths called tow conjugate depth.

Given

YC=2.00m & So1=0.003188 So2=0.0921 & So3=0.0011262

B=4.00m & Z=2.00

Trapezoidal section

Required

1- tow conjugate depth

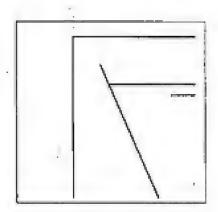
2- relative initial and sequent depth

3- jump losses and efficiency

4- jump length

5- drawing water surface profile

Solution



$$\frac{Q^{2}}{g} = \frac{A^{3}}{T}$$

$$\frac{Q^{2}}{9.81} = \frac{[y(b+zy)]^{3}}{b+2Zy} = \frac{(2(4+2*2))^{3}}{(4+2*2*2)}$$

Q=57.886m3/s

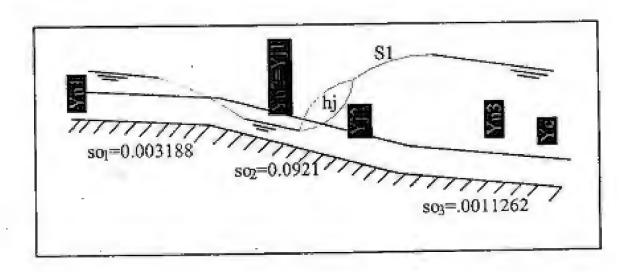
$$4.7669 = \frac{1}{\left(4 + 2y_{\pi 2}\sqrt{1 + (2)^2}\right)^{\frac{3}{4}}}$$

$$Q = \frac{1}{n} * \frac{A^{\frac{5}{2}}}{P^{\frac{3}{2}}} * S^{\frac{1}{2}} ... m^{3} / \sec \dots 57.866 = \frac{1}{0.025} * \frac{\left[y_{n2}(4+2y_{n2})\right]^{\frac{5}{2}}}{\left(4+2y_{n2}\sqrt{1+(2)^{2}}\right)^{\frac{5}{2}}} * (0.0011262)^{\frac{5}{2}}$$

$$43.108 = \frac{\left[y_{n2}(4 \div 2y_{n2})\right]^{\frac{5}{2}}}{\left(4 \div 2y_{n2}\sqrt{1 + (2)^{2}}\right)^{\frac{5}{2}}}$$

yn3=3.00m

Assume S1 occur



$$FI_1 = \frac{V_1}{\sqrt{g^* y_{01}}}$$

$$V_1 = \frac{Q}{A_1} = \frac{57.866}{1.00(4 + 2 * 1.00)} = 9.644 m/s$$

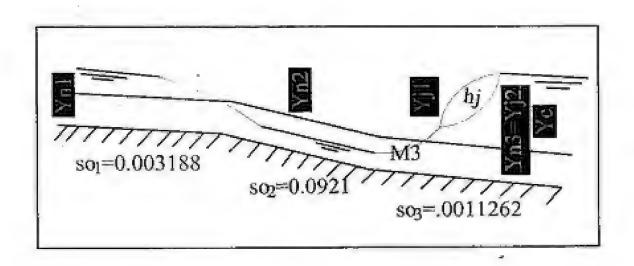
$$y_{ki} = \frac{A}{T} = \frac{1.00 * (4 + 2 * 1.00)}{(4 + 2 * 2 * 1.00)} = 0.75m$$

$$FI_1 = \frac{9.644}{\sqrt{9.81*0.75}} = 3.556 > 1.00....super...eritical..flow$$

$$\frac{y_2}{y_1} = \frac{1}{2} (\sqrt{1 + 8FI_1^2} - 1.00)$$

$$\frac{y_2}{1.00} = \frac{1}{2} (\sqrt{1 + 8*(3.556)^2} - 1.00)$$

 $y_{j2} = 4.554m > y_{n2}....M_3...OCCUR$



Y2j=yn3=3.00m

$$FI_2 = \frac{V_3}{\sqrt{g^* y_{k2}}}$$

$$V_2 = \frac{Q}{A_{21}} = \frac{57.866}{3.00(4 + 2^* 3.00)} = 1.929 m/s$$

$$y_{h2} = \frac{A_2}{T} = \frac{3.00*(4+2*3.00)}{(4+2*2*3.00)} = 1.875m$$

$$FI_2 = \frac{1.929}{\sqrt{9.81*1.875}} = 0.4498 \prec 1.00....sub...eritical..flow$$

$$\frac{y_1}{y^2} = \frac{1}{2} (\sqrt{1 + 8FI_2^2} - 1.00)$$

$$\frac{y_1}{3.00} = \frac{1}{2} (\sqrt{1 + 8 * 0.4498^2} - 1.00)$$

$$y_{ij} = 0.927m$$

$$E_1 = y_1 + \frac{Q^2}{2g * A_1^2} = 0.927 + \frac{(57.866)^2}{2 * 9.81 * [0.927(4 + 2 * 0.927)]^2} = 5.427$$

$$E_2 = y_2 + \frac{Q^2}{2g * A_2^2} = 3.00 + \frac{(57.866)^2}{2 * 9.81 * [3.00 * (4 + 2 * 3.00)]^2} = 3.019m$$

2 - Relative. Initial... Depth =
$$\frac{y_1}{E_1} = \frac{3.00}{6.74} = 0.445$$

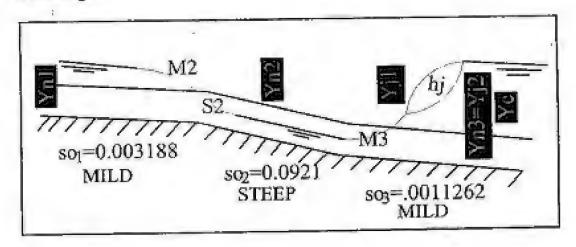
2 - Relative. sequent... Depth =
$$\frac{y_1}{E_1} = \frac{0.927}{6.74} = 0.1375$$

$$3 - head...losses......h_t = E1 - E2 = 6.74 - 3.019 = 3.721m$$

$$3 - efficiency...of....jump = \frac{\gamma * Q * h_L}{75} = \frac{1000 * 57.866 * 3.721}{75} = 2870.93HP$$

$$4 - Lenght...of....jump = 5.20*hj = 5.20*(3.00-0.926) = 10.785m$$

5-Drawing

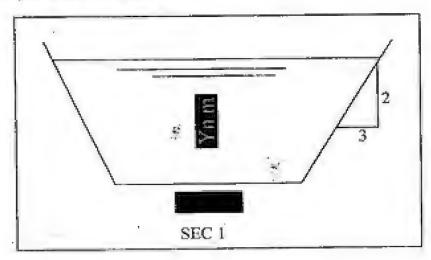


Given

S=0.009 n=0.025 8.

Q=450m3/s Z=1.50

Trapezoidal section



Required

S= 900cm/km

2-

118.585 =
$$\frac{\left[y_{s}(20+1.50y_{s2})\right]^{\frac{5}{5}}}{\left(20+3.61y_{s}\right)^{\frac{2}{5}}}$$

By trial and error

$$Y_n = 2.83m$$

$$3-y_{k} = \frac{A}{T} = \frac{2.83*(20+1.50*2.83)}{(20+2*1.50*2.83)} = \frac{68.6134}{28.49} = 2.408m$$

 $Y_h = 2.408m$

$$4-FI = \frac{v}{\sqrt{g * y_h}} = \frac{|450/68,6134|}{\sqrt{9.81 * 2.408}} = 1.349....sup er...critical...flow$$

FI=1.349 flow super critical

5-
$$R = \frac{A}{P} = \frac{[68.6133]}{[20 + 2 \cdot 2.83\sqrt{1 + (1.50)^{\frac{2}{5}}}]} = \frac{68.6133}{30.204} = 2.272$$

$$IR = \frac{V \cdot R}{D} = \frac{(450/68.613) \cdot (2.272)}{1 \cdot 10^{-6}} = 14,900,966.29 \succ 2000.....turbulent...flow$$

IR=14,900,966.29 flow turbulent

Flow super critical turbulent

6-
$$\frac{Q^2}{g} = \frac{A^3}{T} \qquad \frac{(450)^2}{9.81} = \frac{[y_e(b+zy_e)]^3}{b+2Zy_e} = \frac{(y_e(20+1.50*y_e))^3}{(20+2*1.50*y_e)}$$

$$20,642.20 = \frac{(y_e(20+1.50*y_e))^3}{(20+2*1.50*y_e)}$$

By trial and error

Y_c=3.403m>2.83 steep slope

7-
$$y_{k} = \frac{A}{T} = \frac{4.50 * (20 + 1.50 * 4.50)}{(20 + 2 * 1.50 * 4.50)} = \frac{120.375}{33.50} = 3.5932m$$

$$FI = \frac{V}{\sqrt{g * y_{k}}} = \frac{\left[\frac{450}{120.375}\right]}{\sqrt{9.81 * 3.5932}} = 0.6296 < 1.00.....sub...critical...flow$$

FI=0.6296 flow sub critical

$$R = \frac{A}{P} = \frac{\left[120.375\right]}{\left[20 + 2 * 4.50\sqrt{1 + (1.50)^2}\right]} = \frac{120.375}{36.225} = 3.323$$

$$IR = \frac{V * R}{v} = \frac{\left(450\sqrt{120.375}\right) * (3.323)}{1 * 10^{-5}} = 12,422,429.29 \times 2000.....turbulent...flow$$

R=12,422,429.29 flow turbulent Flow sub critical turbulent

8-

Hydraulic jump occur U/S the weir

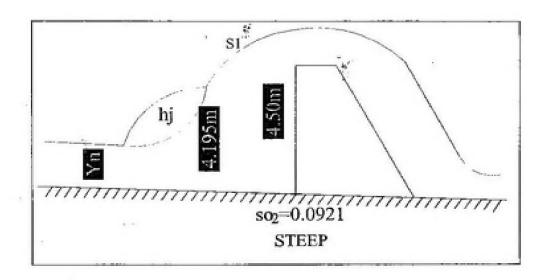
9-

Yj1=yn=2.83

10-

This slope is steep so

S1 occur



$$\frac{y_2}{y_1} = \frac{1}{2} (\sqrt{1 + 8FI_1^2} - 1.00)$$

$$\frac{y_2}{2.83} = \frac{1}{2} (\sqrt{1 + 8 * (1.349)^2} - 1.00)$$

Y2=4.166m

11-

This slope is steep

12-

Water surface profile U/S the weir

13

$$E_1 = y_1 + \frac{Q^2}{2g * A_1^2} = 4.195 + \frac{(450)^2}{2 * 9.81 * [4.195(20 + 1.50 * 4.195)]^p} = 5.0435$$

E1=5.0435m

14-

$$E_1 = y_2 + \frac{Q^2}{2g * A_2^2} = 4.50 + \frac{(450)^2}{2 * 9.81 * [4.50 * (20 + 1.50 * 4.50)]^2} = 5.212m$$

E2=5.212m

$$\Delta E = E$$
, $-E1 = 5.212 - 5.0435 = 0.1685m$

Δ E=0.1685m

16-

$$450 = \frac{1}{0.025} * \frac{\left[4.195(20 + 1.50 * 4.195)\right]^{\frac{2}{5}}}{\left(20 + 2 * 4.195 * \sqrt{1 + (1.50)^{2}}\right)^{\frac{2}{5}}} * \left(SO_{1}\right)^{\frac{1}{2}}$$

$$450 = \frac{1}{0.025} * \frac{[110.29)^{\frac{2}{3}}}{[35.125]^{\frac{2}{3}}} * (SO_1)^{\frac{1}{2}}$$

$$SO1 = 2.262*10^{-3}$$

$$450 = \frac{1}{0.025} * \frac{\left[4.50(20 + 1.50 * 4.50)\right]_{5}^{2}}{\left(20 + 2 * 4.50\sqrt{1 + (1.50)^{2}}\right)_{5}^{2}} * \left(SO_{2}\right)_{2}^{2}$$

$$450 = \frac{1}{0.025} * \frac{[120.375)^{\frac{1}{2}}}{[36.225]^{\frac{2}{3}}} * (SO_2)^{\frac{1}{2}}$$

SO2 =1.7614*10⁻³

$$SE_{AVE}$$
= (SO1+ SO2)/2
= (2.262*10³+1.7614*10⁻³)2
=2.0117*10⁻³

SE_{AVE}=2.0117*10⁻³

17-

$$\Delta S = SO - SE_{AVE}$$

= $\cdot \cdot \cdot \cdot \cdot 1 - 2.0117*10^{-3}$
= $6.9983*10^{-3}$
 $\Delta x = \frac{\Delta E}{\Delta S} = \frac{01685}{6.9983*10^{-3}} = 24.078$

18-

$$K = \frac{1}{n} * \frac{A^{\frac{5}{3}}}{P^{\frac{2}{3}}} ... m^{3} / \sec ... K = \frac{1}{0.025} * \frac{\left[2.83(20 + 1.50 * 2.83)\right]^{\frac{5}{3}}}{\left(20 + 2 * 2.83\sqrt{1 + (1.50)^{2}}\right)^{\frac{5}{3}}} = 4742.79 m^{3} / \sec ...$$

K=4742.79 m3/S

$$A = [3.403(20 + 1.50 * 3.403)] = 85.43m_2$$

$$y_k = \frac{A}{T} = \frac{85.43}{(20 + 2 * 1.50 * 3.403)} = \frac{85.43}{30.209} = 2.828m$$

$$Z = A\sqrt{yh} = 85.43 * \sqrt{2.828} = 143.664$$

Or
$$Z = \sqrt{\frac{Q^2}{g}} = \sqrt{\frac{430^2}{9.81}} = 143.664m^{2.5}$$

$Z=143.664m^{2.5}$

| NO | 1 | ۲ | ٣ | ٤ | 0 | ٦ | Y | ٨ | 9 | 1. | 11 | ١٢ | 12 | ١٤ | 10 | 17 | ۱۷ | 14 | 19 |
|--------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|
| answer | C | b | a | С | b | ь | a | a | a | a | b | a | a | a | a | a | a | a | С |